Reducing CO₂ emissions for flights through complex wind fields using three different optimal control approaches.





Map data: Google, Data SIO, NOAA, U.S. Navy, NGA, GEBCO, Image IBCAO, Image Landsat/Copernicus.

Supervisors: Paul D. Williams, Nancy K. Nichols, Dante Kalise, D.I.A. Poll



cathie.wells@reading.ac.uk

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Today's planned route:



Motivation: if it isn't broken...

>Time minimal trajectories using an indirect method

Fixed time trajectories using a direct method

>Free time, fuel minimal trajectories using dynamic programming

➢Future horizons

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 $\sum_{i=1}^{1}$ of all anthropogenic climate change traceable to the aviation industry. (1)

> 905 million tonnes of CO₂ emitted in 2018. (2)

►ICAO: planes to fly "most fuel efficient route".(3)



 \succ "If aviation was a country, it would be in the top ten of emitters." (4)

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cathie.wells@reading.ac.uk

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cathie.wells@reading.ac.uk

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Alternative ideas

Married Woman and State

Change plane design.

Fleets have become 54% more efficient in the last 30 years.(8)









cathie.wells@reading.ac.uk

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Excess Average Fuel Economy [pax-km/L] Fuel/pax-km Norwegian WOW air + 13% SWISS + 19% KLM + 22% + 26% Turkish + 26% Air Franc Thomas Cool + 26% + 26% Virgin Atlantie + 29% Icelandai Iberi + 29% Delta + 29% + 29% Scandinaviar American + 33% Austrian + 33% Aer Lingu + 33% + 33% Alital + 33% Aerofic + 42% Unit + 47% Luftha + 63% British Airway INDUSTRY AVERAGE

Norwegian Named Most Fuel-Efficient Airline on Transatlantic Routes for a Second Time by ICCT

Change plane design.

Fleets have become 54% more efficient in the last 30 years.(8)

Put more passengers on each flight.

Premium passengers: 5.2% of air traffic, but 30.4% of passenger revenue.

Alternative ideas





Alternative ideas

Change plane design.

Fleets have become 54% more efficient in the last 30 years.(8)

Put more passengers on each flight.

Premium passengers: 5.2% of air traffic, but 30.4% of passenger revenue.(8)

Develop flocks of aircraft.

Fine on paper, but delays would cause fuel usage to be impossible to predict.(9,10)





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Alternative ideas

Change plane design.

Fleets have become 54% more efficient in the last 30 years.⁽⁸⁾

> Put more passengers on each flight.

Premium passengers: 5.2% of air traffic, but 30.4% of passenger revenue.(8)

Develop flocks of aircraft.

Fine on paper, but delays would cause fuel usage to be impossible to predict. (9,10)

Invest in development of biofuels.

> Research is starting now and will still only be able to produce one third of the fuel needed by 2050.(11)

, fertilized... [+] GETTY







Motivation: A practical solution



>100% satellite coverage of North Atlantic.



Photo source: Aireon.

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>100% satellite coverage of North Atlantic.

Trajectory Based Operations: better efficiency.



Photo source: Airbus.com



Motivation: A practical solution





≻100% satellite coverage of North Atlantic.

>Trajectory Based Operations: better efficiency.

11:40	XZ 5555	Paris	Delayed
11:45	RT 4545	Montreal	Estimated 11:45
11:50	QE 0900	New York	ESGINIC
11:50	QE 0000	Montevideo	Delayed
11:55	QE 2103	Barcelona	On Time
12:00	SQ 0052	Toronto City	Delayed
12:00	AK 7304	Romo	Delayeu
12:10	AK 8900	Suda cu	On Time
12:15	50 0232	Sydney	Estimated 12.45
12:20	XZ 3170	Hong Kong	Delayod
12:20	SQ 0080	Washington D.C	sciayed
12:30		Tokyo	Delayod

Photo source: travel.stackexchange.com

>Airlines need to reduce emissions, whilst adhering to a schedule.

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Optimal control theory:





Figure 1: Control Theory Map by Brian Douglas, https://engineeringmedia.com/.



Three main methods:

- Indirect methods
- Direct methods
 - Dynamic programming

cathie.wells@reading.ac.uk

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How much difference would horizontal, time optimal trajectory planning make to fuel use and thus carbon dioxide emissions, in fixed airspeed transatlantic flights compared with the Organised Track Structure?



Method:



- ➢ Routes: JFK (40.6°N,73.8°W) and LHR (51.5°N,0.5°W).
- ≻Winter period: 1st December, 2019 to 29th February, 2020.
- Winds from: National Center for Atmospheric Research (2.5° resolution).
- Constant altitude FL340 equating approximately to a pressure of 250 hPa.
- Constant airspeed across each trajectory, from 200 m/s to 270 m/s.
- ≻Air distance: airspeed x flight time.
- > Fuel usage and emissions proportional to air distance.

Defining the spherical system



Defining the symbols:

- λ longitude in radians
- ϕ latitude in radians
- θ heading angle in radians
- u zonal wind in m s⁻¹
- v meridional wind in m s⁻¹
- *V* air speed of aircraft in m s⁻¹
- *R* radius of Earth in m (here approximated to 6 371 000 m)
- t time in seconds



Defining the problem



Parameters:

Boundary conditions: Dynamical system:

 $t_0 = 0$
 $t_{final} \ge 0$

$$\lambda(0) = \lambda_{dept}$$

 $\phi(0) = \phi_{dept}$

$$\dot{\lambda} = \frac{V\cos\theta + u(\lambda,\phi)}{R\cos\phi}$$
$$\dot{\phi} = \frac{V\sin\theta + v(\lambda,\phi)}{R}$$

State variables:

$$x_1 = \lambda(t)$$

$$x_2 = \phi(t)$$
Control variable
$$\alpha(t) = \theta$$

$$\boldsymbol{\alpha}(t) = \boldsymbol{\theta}$$

$$J(\boldsymbol{x}, \alpha) = \int_{t_0}^{t_{final}} 1 \, dt = t_{final}$$

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Method: Euler Forward Step



$$\frac{d\lambda}{dt} = \frac{V\cos\theta + u(\lambda,\phi)}{R\cos\phi} \qquad \qquad lo_{t+1} = lo_t + \frac{u_t + V\cos he_t}{R\cos la_t} \times dt$$
$$\frac{d\phi}{dt} = \frac{V\sin\theta + v(\lambda,\phi)}{R} \qquad \qquad la_{t+1} = la_t + \frac{v_t + V\sin he_t}{R} \times dt$$

$$\frac{d\theta}{dt} = -\frac{1}{R\cos\phi} \left[-\sin\theta\cos\theta\frac{\partial u}{\partial\lambda} + u\cos^2\theta\sin\phi + \cos^2\theta\cos\phi\frac{\partial u}{\partial\phi} - \frac{\partial v}{\partial\lambda} + \cos^2\lambda\frac{\partial v}{\partial\lambda} \dots \right] he_{t+1} = he_t - \frac{Wind \times dt}{R\cos la_t} + v\sin\theta\cos\theta\sin\phi + \sin\theta\cos\theta\cos\phi\frac{\partial v}{\partial\lambda} + V\cos\theta\sin\phi \right]$$

$$Wind = -\sin he_t \cos he_t \left(\frac{du}{dlo}\right)_t + u \cos^2 he_t \sin la_t + \cos^2 he_t \cos la_t \left(\frac{du}{dla}\right)_t \dots - \left(\frac{dv}{dlo}\right)_t + \cos^2 lo_t \left(\frac{dv}{dlo}\right)_t + v \sin he_t \cos he_t \sin la_t \dots$$

+ sin $he_t \cos he_t \cos la_t \left(\frac{dv}{dla}\right)_t$ +V cos $he_t \sin la_t$

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(a) Air distances 1st December, 2019 westbound

(b) Air distances 1st December, 2019 eastbound

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Results: Savings





Unweighted data:

Assumes equal numbers of flights along each track supplied by NATS each day. Savings found by taking average air distance change over each track, each day.

Weighted data:

Uses information supplied by NATS to show how many aircraft used each track each day. Savings are found by a weighted average of air distance savings across all tracks each day.

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Overview of Findings:

Route	% improvement		
	Best	Worst	
JFK to LHR	0.9	16.4	
LHR to JFK	1.1	7.8	

Route	% improvement at 240 m/s	
	Weighted Average	
JFK to LHR	2.5	
LHR to JFK	1.7	









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JFK to LHR	2.5	
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Fixed time trajectories using a direct method:

Can fixed time flights be planned for a whole winter season to ensure that fuel is minimised?

In minimising fuel burn of transatlantic flights, can extra benefits result from controlling airspeed in addition to heading angle?

$$g = \frac{W \times V_{\infty}}{\eta_0 \frac{L}{D} \times LCV}$$

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(15,16)

Involves:

- aircraft parameters
- ISA atmospheric parameters
- altitude
- airspeed
- temperature

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Method: Assumptions



- ➢ Routes: JFK (40.6°N,73.8°W) and LHR (51.5°N,0.5°W).
- > Winter period: 1st December, 2019 to 29th February, 2020.
- > Winds and temperature from: National Center for Atmospheric Research
- > 2.5° resolution.
- > Constant pressure of 250 hPa equating approximately to FL340.

Fixed time West 29 000 s, fixed time East 22 000 s.

Mass of aircraft varies as fuel is burned.

Fuel burn function based on recent papers by Poll and Schumann (15,16).

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Optimal control problem 2



Parameters:

$$\begin{aligned} t_0 &= 0 \\ t_{final} &= t_f \end{aligned} \qquad t \in [0, t_f] \subset \mathbb{R}$$

Boundary conditions:

 $\lambda(0) = \lambda_{dept}$ $\phi(0) = \phi_{dept}$ $M(0) = M_{dept}$

State variables:

Control variable:

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Optimal control problem 3



Parameters:

$$t_0 = 0 \qquad t \in [0, t_f]$$
$$t_{final} = t_f$$

State variables:

 $\subset \mathbb{R}$

Boundary conditions:

 $\lambda(0) = \lambda_{\mathsf{dept}}$ $\phi(0) = \phi_{\mathsf{dept}}$ $M(0) = M_{dept}$

Control variables:

 $x_1 = \lambda(t)$ $x_2 = \phi(t)$ $x_3 = M(t)$

$$\pmb{x}(t) {:} [0, t_f] \mapsto \mathbb{R}^3$$

$$\alpha_1(t) = \theta$$
$$\alpha_2(t) = V$$

 $\boldsymbol{\alpha}(t): [0, t_f] \mapsto \mathbb{R}^2$

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OCP 2 and 3:



Dynamical systems:

$$\dot{x}_{1} = \frac{V \cos \alpha + u(x_{1}, x_{2})}{R \cos x_{2}}$$
$$\dot{x}_{2} = \frac{V \sin \alpha + v(x_{1}, x_{2})}{R}$$
$$\dot{x}_{3} = -g(x_{1}, x_{2}, x_{3})$$

Cost functionals:

$$J(\boldsymbol{x}, \alpha) = \int_{t_0}^{t_{final}} g(\boldsymbol{x}) dt$$

$$\dot{x}_{1} = \frac{\alpha_{2} \cos \alpha_{1} + u(x_{1}, x_{2})}{R \cos x_{2}}$$
$$\dot{x}_{2} = \frac{\alpha_{2} \sin \alpha_{1} + v(x_{1}, x_{2})}{R}$$
$$\dot{x}_{3} = -g(x_{1}, x_{2}, x_{3}, \alpha_{2})$$

$$J(\mathbf{x}, \boldsymbol{\alpha}) = \int_{t_0}^{t_{final}} g(\mathbf{x}, \boldsymbol{\alpha}_2) dt$$

cathie.wells@reading.ac.uk

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Flying East:

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More tailwind along GCR, more variability

in airspeed.

 $V \le 201.5$ $211.5 \le V < 214$ $224 \le V < 226.5$ $201.5 \le V < 204$ $214 \le V < 216.5$ $226.5 \le V < 229$ $204 \le V < 206.5$ $216.5 \le V < 219$ $229 \le V < 231.5$ $206.5 \le V < 209$ $219 \le V < 221.5$ $231.5 \le V < 234$ $209 \le V < 211.5$ $221.5 \le V < 224$ $234 \le V < 236.5$

Key to Airspeeds (V m/s) :



Results: Air speed changes







Overview of Findings:

Daily variation in savings across winter season 2019-2020

cathie.wells@reading.ac.uk	cathie.we	lls@reading.ac.uk	
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Fuel savings in kg made by controlling airspeed in addition to heading angle

Westbound

Eastbound

Free time, fuel minimal trajectories using dynamic programming:



Would minimising fuel, but allowing time to be free, in a fixed altitude flight produce trajectories that are more fuel efficient than those currently flown and to what extent would the flight duration be changed?



Optimal control problem 4 :



Parameters:

$$t_0 = 0 \qquad t \in [0, t_f] \subset \mathbb{R}$$
$$t_{final} = t_f \ge 0$$

State variables:

 $\lambda(0) = \lambda_{dept}$ $\phi(0) = \phi_{dept}$ $M(0) = M_{dept}$

Control variables:

$$x_1 = \lambda(t)$$
$$x_2 = \phi(t)$$
$$x_3 = M(t)$$

$$\boldsymbol{x}(t) : [0, t_f] \mapsto \mathbb{R}^2$$

$$\alpha_1(t) = \theta$$
$$\alpha_2(t) = V$$

 $\boldsymbol{\alpha}(t): [0, t_f] \mapsto \mathbb{R}^2$

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Optimal control problem 5:



Parameters:

$$t_0 = 0 \qquad t \in [0, t_f] \subset \mathbb{R}$$

$$t_{final} = t_f \ge 0$$

Boundary conditions:

$$\lambda(0) = \lambda_{\mathsf{dept}}$$

 $\phi(0) = \phi_{\mathsf{dept}}$

State variables:

Control variables:

$$x_1 = \lambda(t)$$
$$x_2 = \phi(t)$$

$$\boldsymbol{x}(t) \colon [0, t_f] \mapsto \mathbb{R}^2$$

$$\alpha_1(t) = \theta$$
$$\alpha_2(t) = V$$

$$\boldsymbol{\alpha}(t)$$
: $[0, t_f] \mapsto \mathbb{R}^2$

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Optimal control problem 4:



Dynamical system:

$$\dot{x}_1 = \frac{\alpha_2 \cos \alpha_1 + u(x_1, x_2)}{R \cos x_2}$$
$$\dot{x}_2 = \frac{\alpha_2 \sin \alpha_1 + v(x_1, x_2)}{R}$$
$$\dot{x}_3 = -g$$

Cost functional:

$$J(\mathbf{x}, \boldsymbol{\alpha}) = \int_{t_0}^{t_{final}} L(\mathbf{x}, \boldsymbol{\alpha}) dt = \int_{t_0}^{t_{final}} g(\mathbf{x}, \boldsymbol{\alpha}_2) dt$$

$$J(t): [0, t_f] \times \mathbb{R}^3 \times \mathbb{R} \mapsto \mathbb{R}$$

cathie.wells@reading.ac.uk

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Optimal control problem 5:



Dynamical system:

$$\dot{x}_1 = \frac{\alpha_2 \cos \alpha_1 + u(x_1, x_2)}{R \cos x_2}$$
$$\dot{x}_2 = \frac{\alpha_2 \sin \alpha_1 + v(x_1, x_2)}{R}$$

Cost functional:

$$J(\mathbf{x}, \boldsymbol{\alpha}) = \int_{t_0}^{t_{final}} L(\mathbf{x}, \boldsymbol{\alpha}) dt = \int_{t_0}^{t_{final}} 1 dt$$

$$J(t):[0,t_f]\times \mathbb{R}^2\times \mathbb{R}\mapsto \mathbb{R}$$

cathie.wells@reading.ac.uk

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Dynamic programming: [17]



Solve the Hamilton Jacobi Bellman Equation:

Time minimal:

$$\begin{split} v(x) + \sup_{\alpha \in \mathcal{A}} \{ -Dv \cdot f(x, \alpha) - 1 \} &= 0 \quad x \in \mathbb{R}^N \setminus C \\ v(x) &= 0 & \forall x \in C & \\ \end{split} \quad v(x) := \begin{cases} 1 & T(x) = +\infty \\ 1 - e^{-T(x)} & T(x) < +\infty \end{cases} \end{split}$$

Fuel minimal:

$$V(x) - \inf_{\alpha \in \mathcal{A}} \{g(x, \alpha) + f(x, \alpha) \cdot \Delta V(x) - (g(x, \alpha) - 1)V(x)\} = 0 \quad x \in \mathbb{R}^n \setminus C$$
$$V(x) = 0 \qquad \qquad x \in C$$

Use value function map to find optimal feedback control

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Semi-Lagrangian Scheme: (time)

Updated value for space node *i* and iteration *m*.

I represents linear interpolation of value function outside of grid points.

$$[V]_{i}^{m+1} = \min_{a \in \mathcal{A}} \{ e^{-\Delta t} I[V]_{i}^{m} (y_{i} + \Delta t f(y_{i}, a)) \} + 1 - e^{-\Delta t}$$

Value is calculated for all combinations of control variable and minimum accepted as the node value.

c.a.wells@pgr.reading.ac.uk

Here the dynamical system is approximated by an Euler scheme with time step Δt .

$$V^{\Delta t}(x) := \begin{cases} 1 & T(x) = +\infty \\ & 1 - e^{-\Delta t N(x)} & \text{else} \end{cases}$$

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else

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Semi-Lagrangian Scheme: (fuel)

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Updated value for space node *i* and iteration *m*.

I represents linear interpolation of value function outside of grid points.

$$[V]_{i}^{m+1} = \min_{a \in \mathcal{A}} \{ I[V]_{i}^{m}(y_{i} + \Delta t f(y_{i}, a)) + \Delta t g(y_{i}, \alpha)(1 - V_{i}^{m}(y_{i})) \}$$

Value is calculated for all combinations of control variable and minimum accepted as the node value.

The fuel burn function g is now included in the formulation.

The extra term is included to account for the fact that the running cost is no longer 1 as in the time minimal version.

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Algorithm to find value map:





Actual flight data



Positions and times recorded by flightradar24.com.

>Using wind field and ground speed, airspeed can be recovered.

>If outside practical bounds, adjusted and time altered accordingly.

Altitude kept to approximately FL 340 (barometric pressure of 250 hPa).

Fuel burn calculated as for simulated flights.

Flights from : American Airlines

British Airways

Delta Air Lines

Virgin Atlantic

> 1547 eastbound and 1567 westbound flights considered.



Results: comparison across all data

At 5% level: significantly less fuel used, but time of flight not significantly longer. Significantly lower average airspeeds for flights.

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cathie.wells@reading.ac.uk
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Results: comparison across all data





Similar to Eastbound results. Slightly reduced fuel savings and not such a disparity in airspeed.

cathie.wells@reading.ac.uk

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Results: differences between airlines

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Overview of free-time, fuel minimal results:

Total fuel reduction Eastbound: 2.5 million kg
 Total fuel reduction Westbound: 2.8 million kg
 Each 1kg of aviation fuel burned produces 3.16 kg of CO₂
 Across this one winter period :

16.6 million kg reduction in CO₂ emissions

1 307 average UK residents



15 962 average Pakistan residents



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Conclusions:



- Planning transatlantic flights exploiting available winds reduces emissions.
- Reduction of 6.7 million kg of CO₂ emissions on the route between JFK to LHR one winter [20].
- Fuel minimisation for a fixed time route may be more practical than minimising time.
- Altering airspeed can save an extra 723 000 kg of CO₂ emissions compared with just altering heading for fixed-time, fuel minimal routes [21].
- Fuel minimal free-time flights compared with actual flight data:
 16.6 million kg CO₂ emissions saved.
- This is a 4.6% saving flying East and a 3.8% saving flying West.



New Horizons:



- Controlling cruise altitude.
- Including climb and descent phases.
- Avoiding areas of convection and/or super saturated icy regions.
- Training neural networks for faster rerouting as new information becomes available.

Results so far published in Environmental Research Letters (20), Optimization and Engineering (21) and Transportation Research Part D (Transport and Environment) (22).

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